

U.S. Department of Energy

# HelioCon

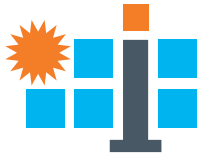
Heliostat Consortium for  
Concentrating Solar-Thermal Power

# Impact of Heliostat Array Density on Boundary Layer Characteristics and Wind Loading

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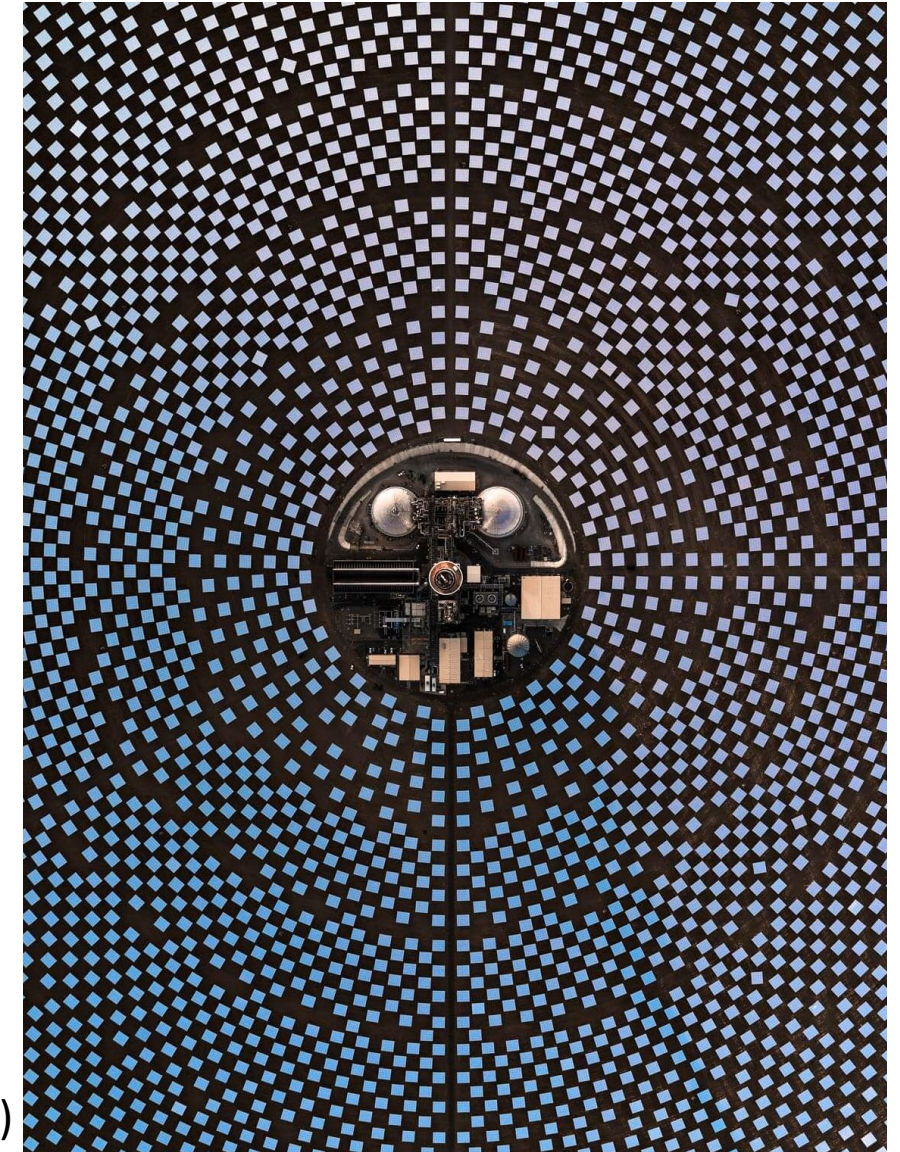
16 July 2024 • ASME ES2024 • Anaheim

conceptual design • components • integration • mass production • heliostat field

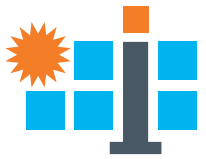


# Introduction

- Heliostat arrangement optimised for optical performance
- Arrangement based on wind loading is not considered
- Heliostat structure overdesigned
- Significant proportion of capital cost
- Heliostats identical in design throughout field
- Change in density with distance from tower and field layout

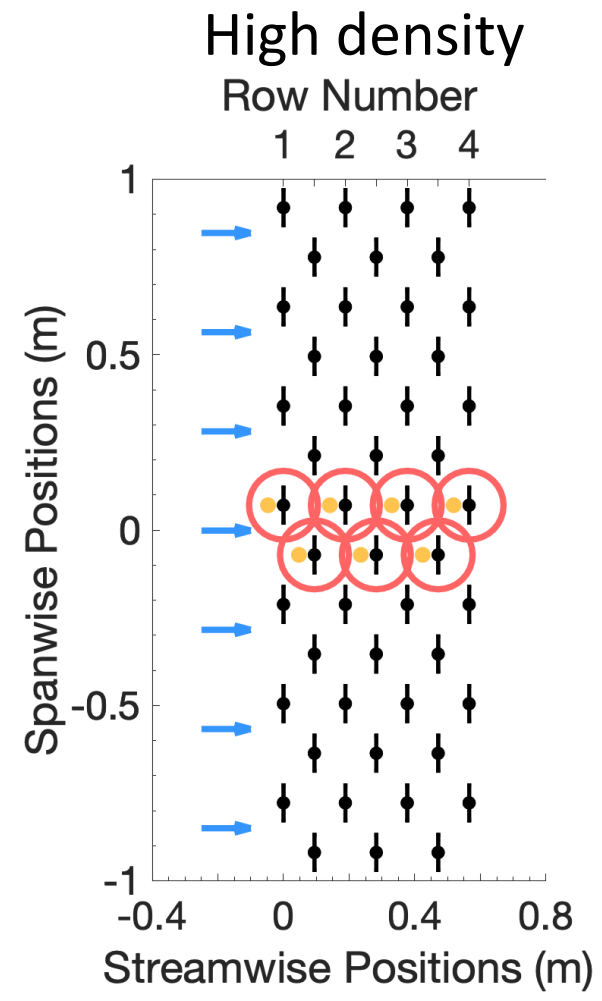
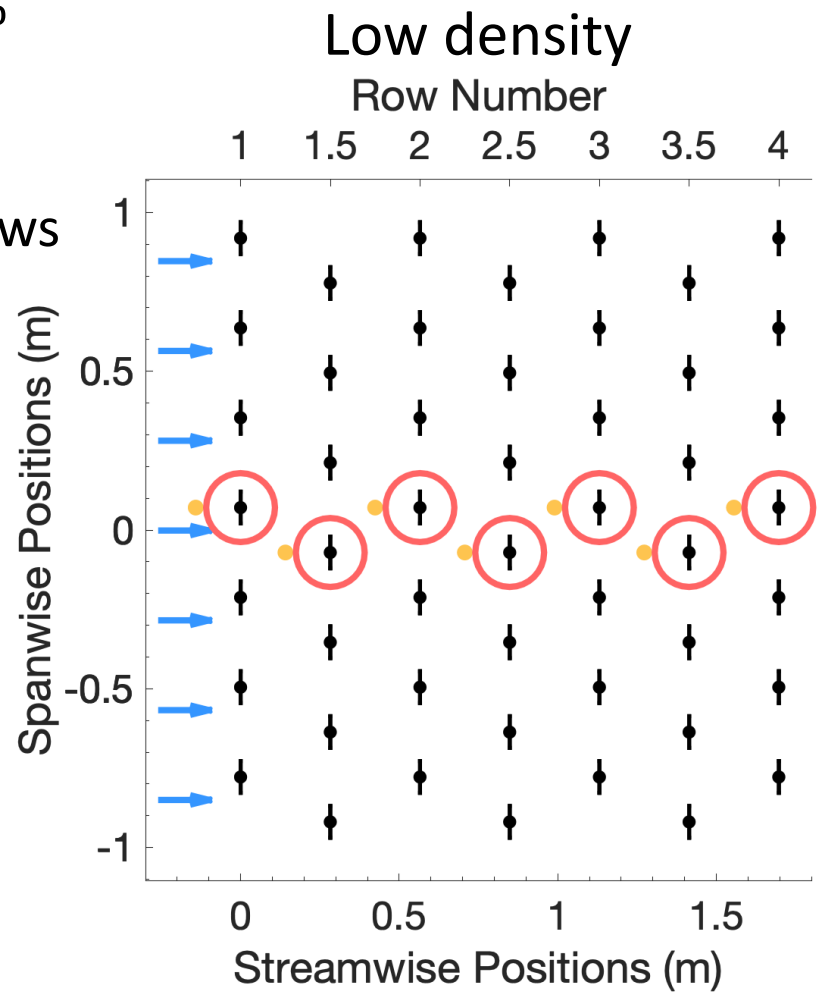
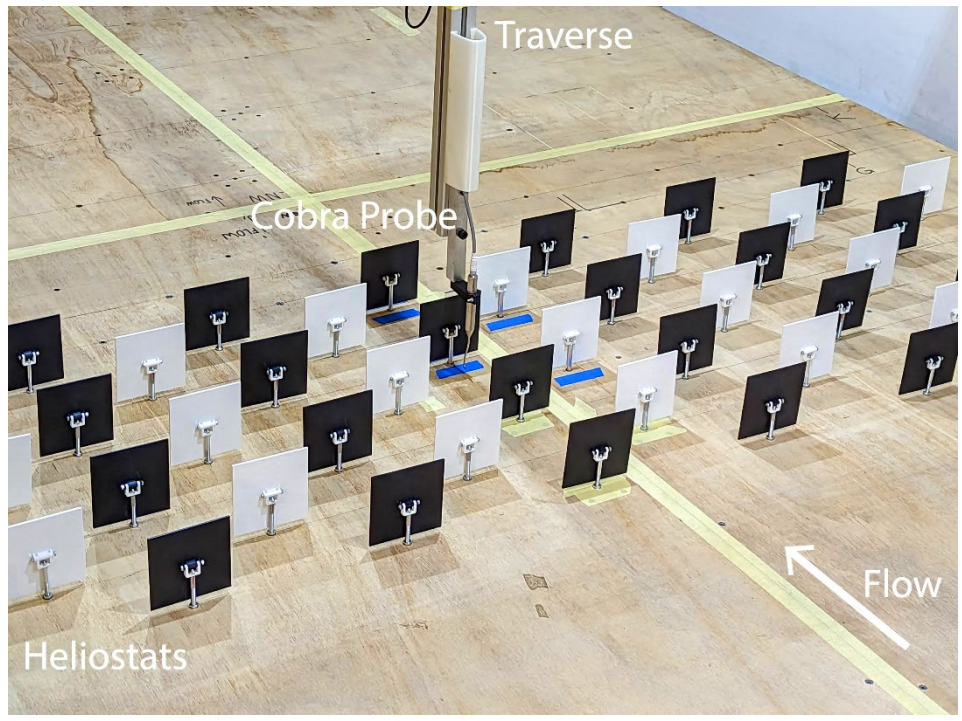


Crescent Dunes 110MW. Photo captured by Hegen (2016)



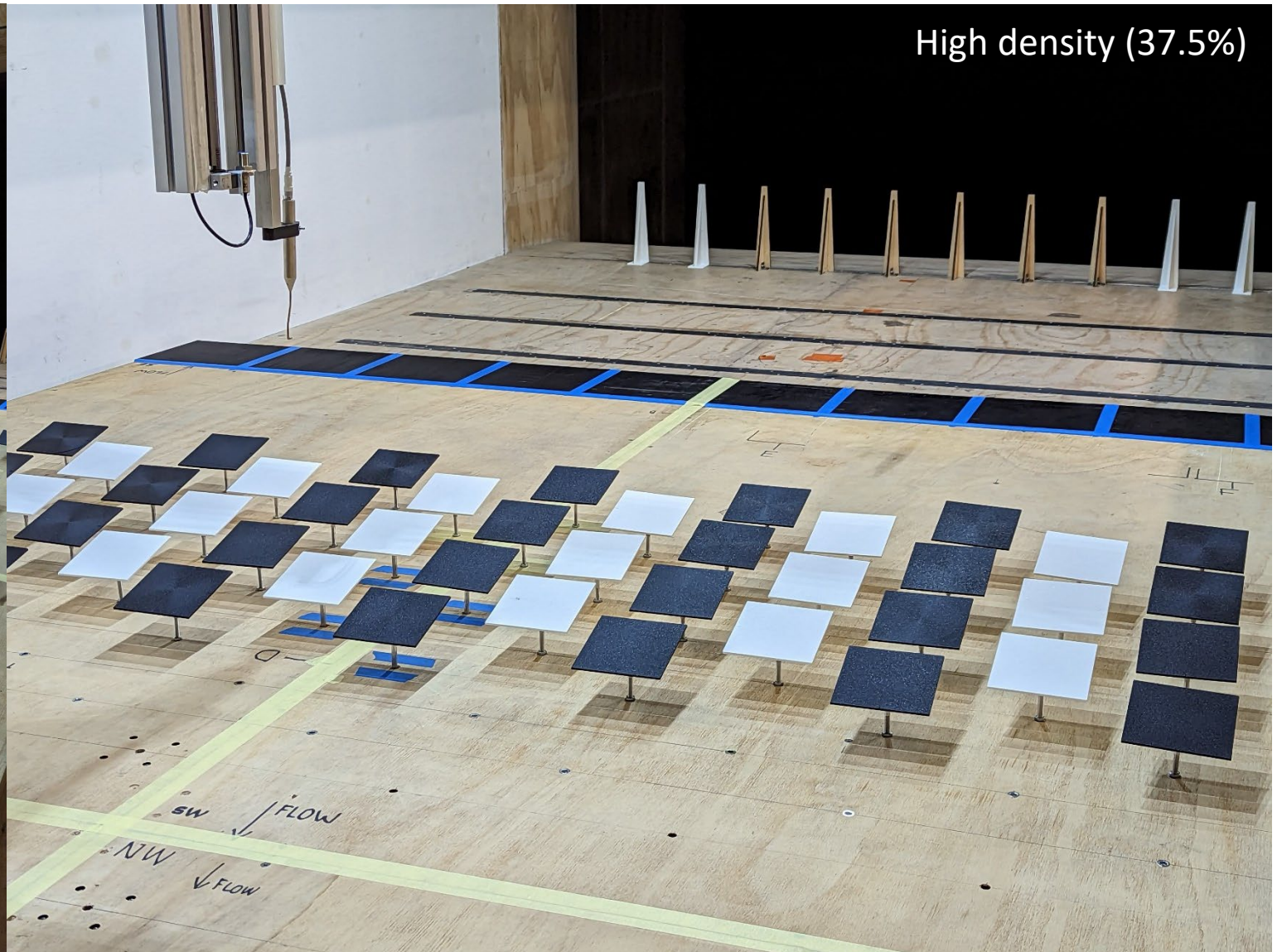
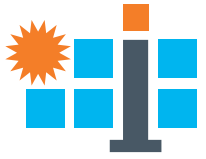
# Wind tunnel experiments – field array layout

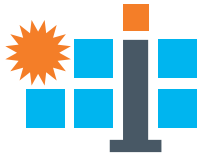
- Field densities of 12.5% (low) and 37.5% (high)
  - Helio­stat aperture area / Ground area
- Flow measurement midway between rows
- Load measurements at each row



○ Load cell location ● Flow measurement location

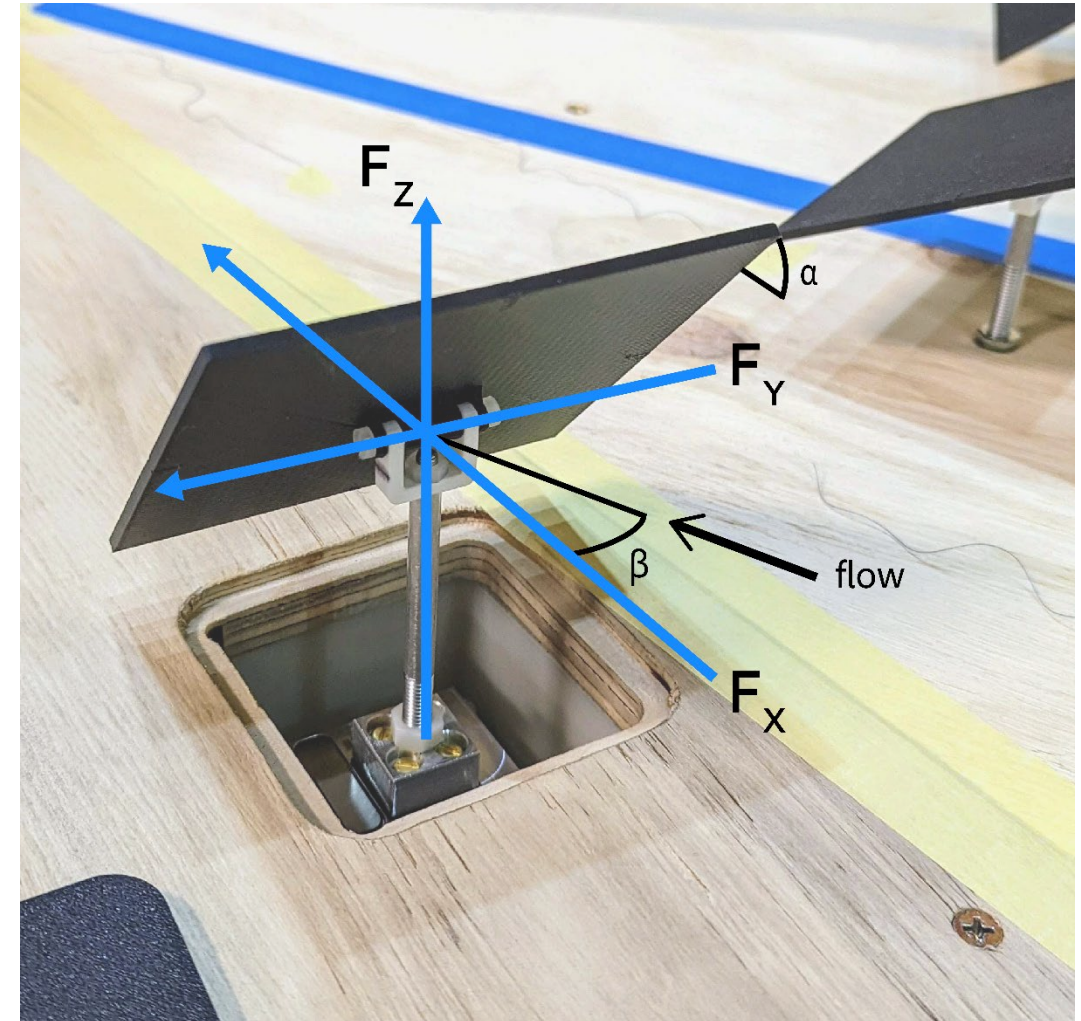
# Comparison of densities

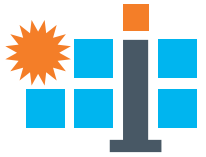




# Wind tunnel experiments – instrumentation

- 3D printed heliostat models with
  - Chord = 0.1 m, Hinge height = 0.075 m
- Adjustable about 3-axes
  - Azimuth ( $\beta$ )
  - Elevation angle ( $\alpha$ )
  - Hinge height
- Four 3-axis  $\pm 2$ N load cell (K3D40)
  - Sampled at 1 kHz simultaneously
  - $F_x, F_y, F_z$  with  $\pm 0.5\%$  accuracy





# Wind tunnel experiments – inflow ABL profiles

- Incoming turbulent flow

- Mean velocity profile

$$U(z) = \frac{u_\tau}{k} \ln \frac{z}{z_0} + d$$

$$u_\tau = 0.5 \text{ m/s}, z_0 = 0.01 \text{ m}, d = 7.75$$

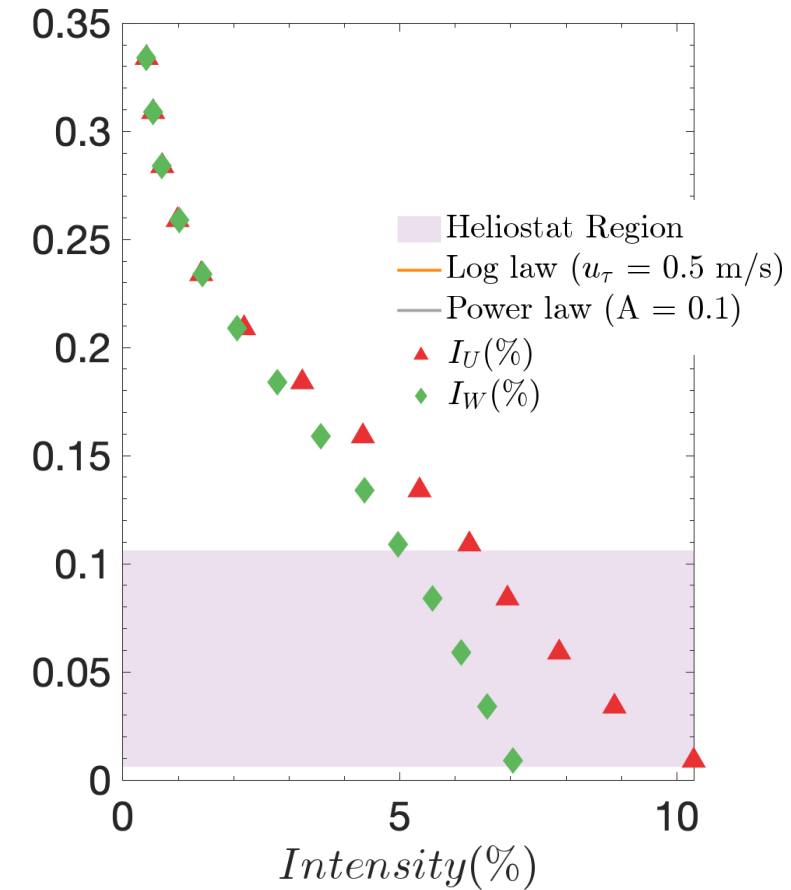
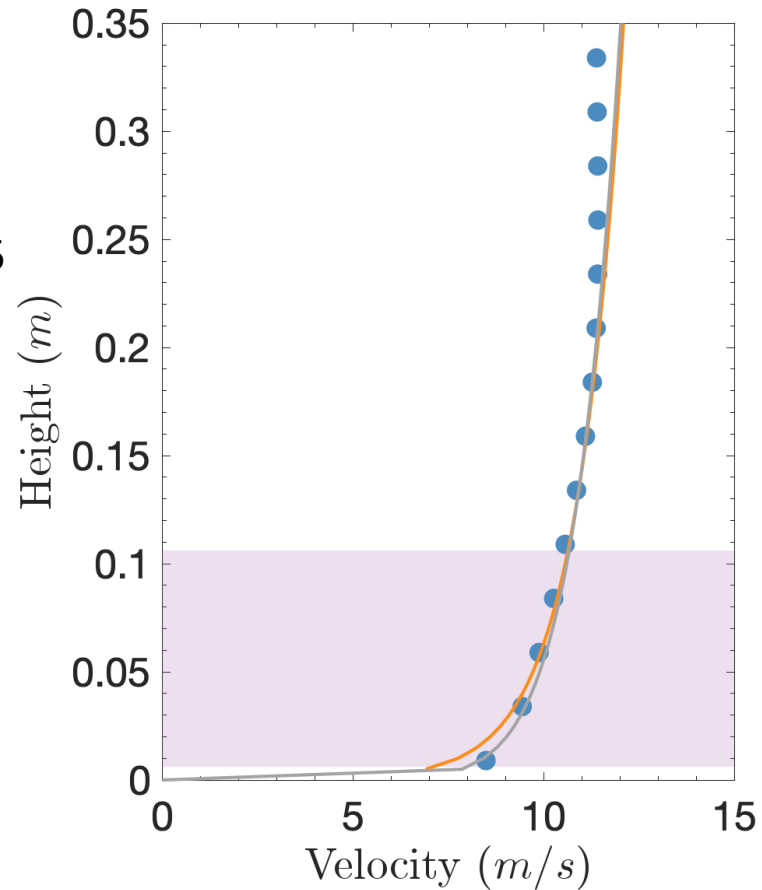
$$U(z) = U_\infty \left( \frac{z}{\delta} \right)^\alpha$$

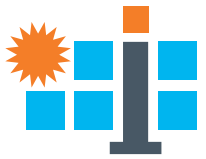
$$U_\infty = 11.4 \text{ m/s}, \delta = 0.2 \text{ m}, \alpha = 0.1$$

- Turbulence intensity profiles

- At hinge height

- 9.8 m/s flow velocity
  - 8% streamwise turbulence
  - 6% vertical turbulence

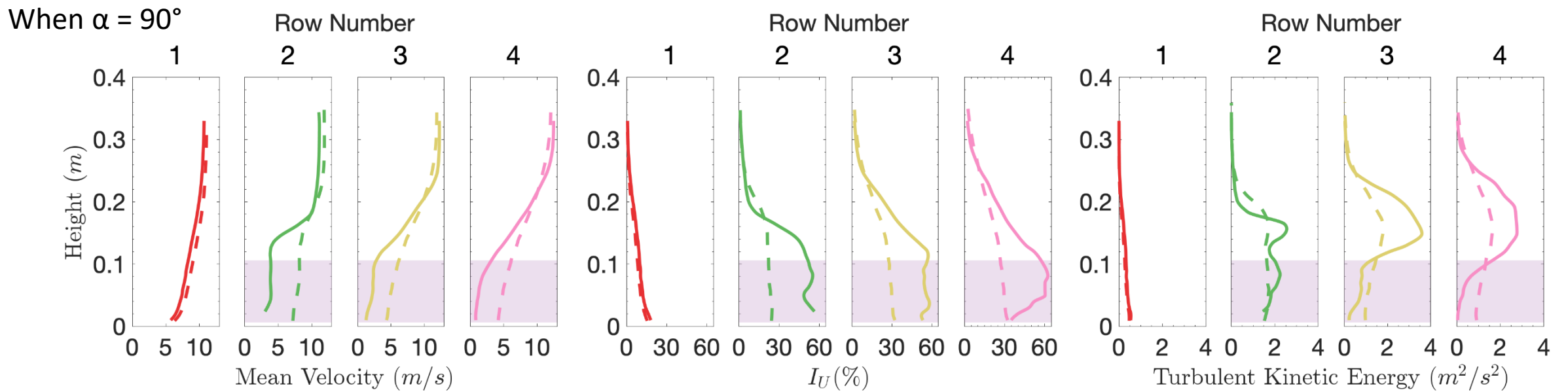




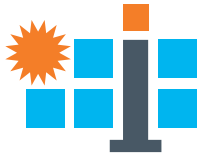
# Effect of field density on flow characteristics

- Reduction in flow velocity within array – similar to canopy flow
- Increase in streamwise turbulence intensity with distance
  - Significant increase for high density case
- Increase in turbulent kinetic energy downstream
  - A reduction in velocity reduces the effect on wind load

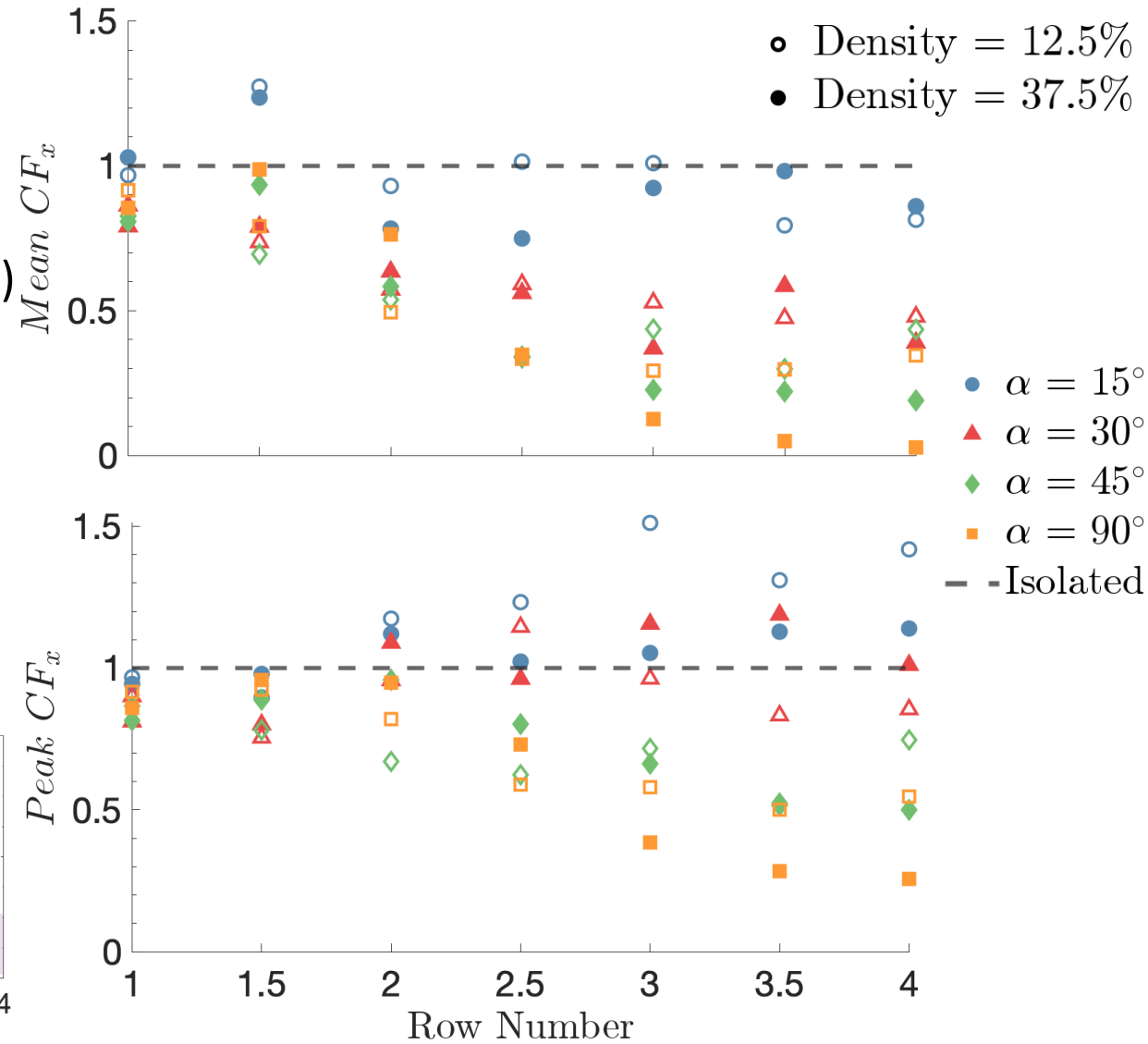
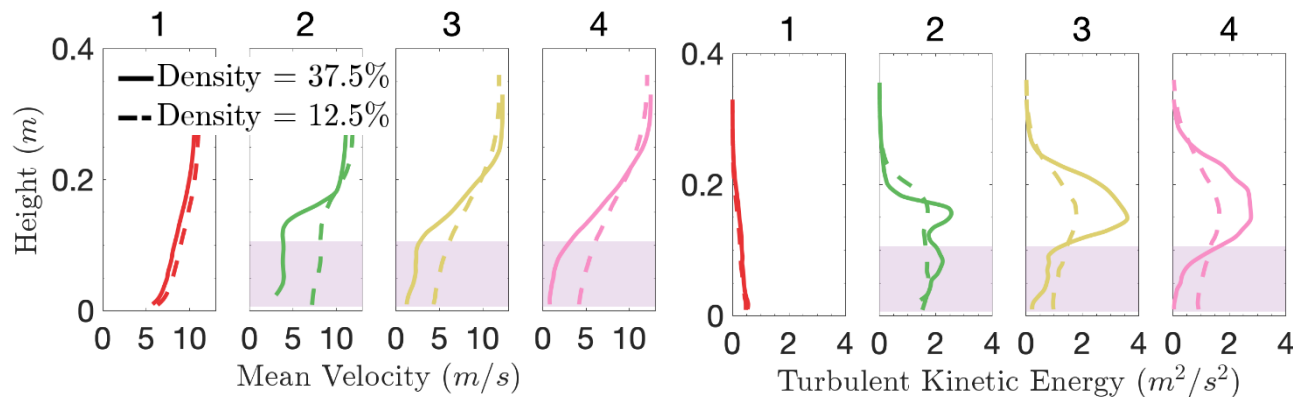
— Density = 37.5%  
 - - Density = 12.5%



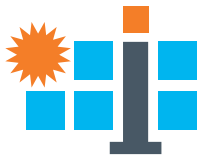
# Effect of field density on drag forces



- Normalised to isolated heliostat drag
- From row 3:
  - Mean and peak reduced by up to 50% ( $\alpha = 90^\circ$ )
  - Increase in density  $\rightarrow$  reduction in drag ( $\alpha \geq 45^\circ$ )
  - Similar drag coefficients at  $\alpha \geq 30^\circ$  (low density)
- Increased peak drag at  $\alpha \leq 30^\circ$
- Maximum mean drag at row 1.5, when velocity and turbulent kinetic energy is high

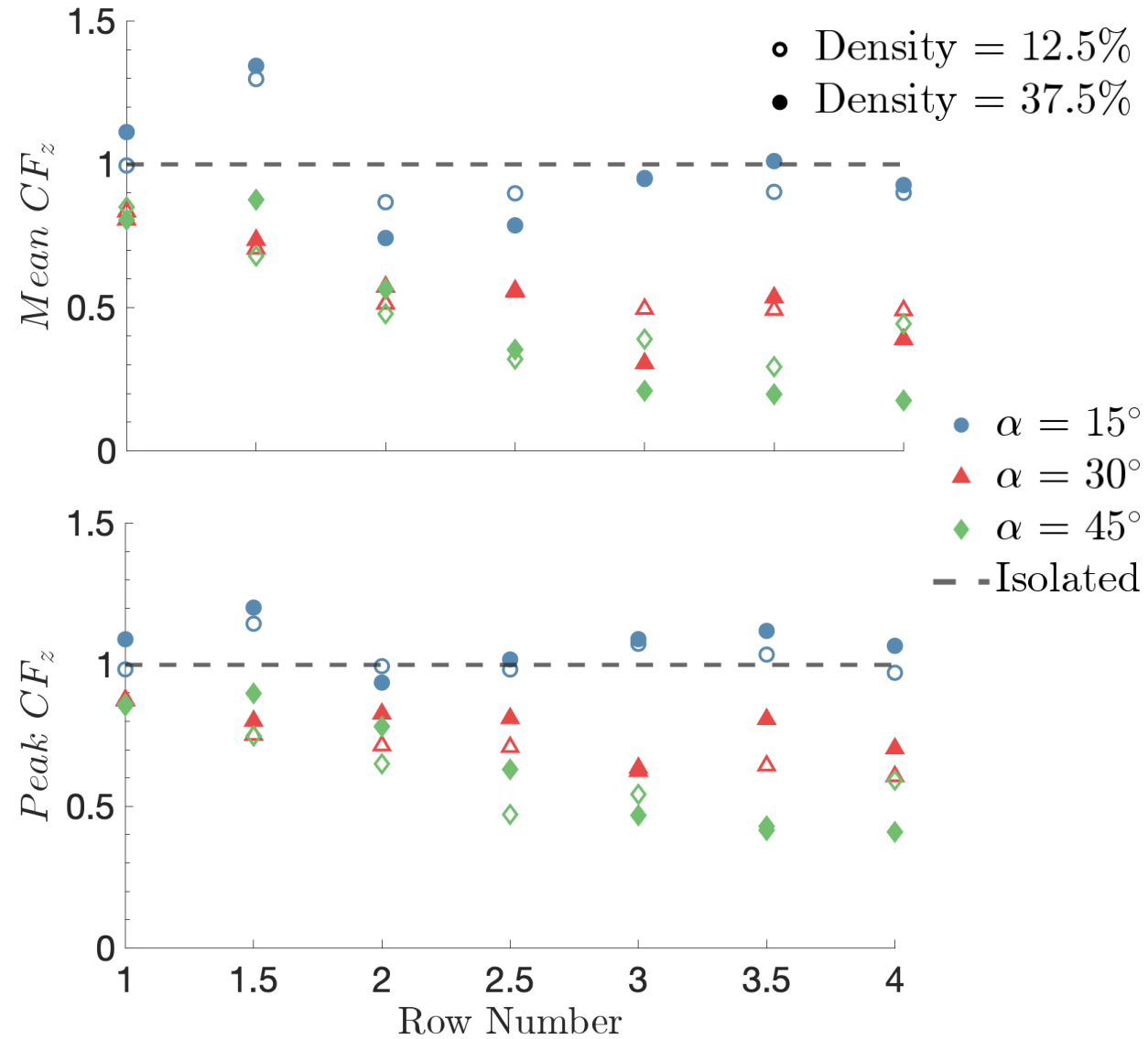


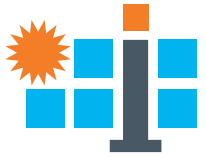




# Effect of field density on lift forces

- Normalised to isolated heliostat lift
- Mean and peak lift at  $\alpha \leq 15^\circ$  remain similar to isolated heliostat
  - Minimal upstream flow blockage
- Amplification of peak lift forces at  $\alpha \leq 15^\circ$  due to channeling flow

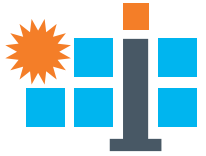




# Conclusions and next steps

- Reduction in drag compared to isolated heliostat
- Fluctuation in mean lift beyond isolated heliostat
- Alternative heliostat design conditions for inner regions
  - Potential for cost reduction
- Investigation into potentially increased hinge moments
- Development of a transformation formula to estimate loads within an array based on individual heliostat investigations

# Acknowledgements



- Heliostat Consortium (HelioCon)

US Department of Energy (DOE) Solar Energy Technologies Office Award DE-EE00038488/38714



- Australian Solar Thermal Research Institute (ASTRI)

Australian Renewable Energy Agency (ARENA) Grant 1-SRI002



Australian Government  
Australian Renewable Energy Agency

- University of Adelaide fabrication and instrumentation teams

